

ON THE RELATIVE EFFICIENCY OF DIFFERENT SHAPED OTTER BOARDS

M. MUKUNDAN, A. V. V. SATYANARAYANA AND H. KRISHNA IYER
Central Institute of Fisheries Technology (Craft & Gear wing), Cochin-5.

Rectangular, Horizontal curved and oval otter boards were tested under identical fishing conditions and their relative efficiency ascertained on the basis of towing tension and the horizontal opening of the boards. While the tension in the warps with the different otter boards was not significant, the horizontal curved board gave increased lateral spread to the net.

INTRODUCTION

Size, shape, rigging and method of attachment of otter boards have constantly attracted the attention of Gear Technologists ever since the advent of this method of fishing and many theories have been propounded. Yakovliev (1955), Gaun—quoted by Dickson (1959), Walderhaug and Akre and Frey and Shore—quoted by Crewe (1963) studied the hydrodynamic properties of flat rectangular boards, while their efficiency in terms of attachment of the bridles were investigated by Takayama and Koyama (1959), Satyanarayana and Mukundan (1962) and Ben yami (1963). Takayama and Koyama (1961) further recorded that otter doors having height larger than the base are relatively more effective. Sevastinov (1955), Yakovliev (1955), Matrosov (1958), Scharfe (1959), Ben yami (1963) and Dale and Moller (1963) investigated the efficiency of the oval otter boards and Knake and Whiteleather (1944), Scharfe (1959), Suber

krub (1958) and Catasta (1959) conducted similar studies on doors having hydrofoil cross section. It is, however, significant to record that the majority of the above investigations were conducted either in a tunnel or testing tank with possibly the works of Scharfe (1959) and Ben yami (*op. cit.*) as the only exceptions. Therefore keeping in view the merits and demerits of otter doors of various types and shapes enquired into elsewhere, experiments to study the relative efficiency of three different types of boards under actual fishing conditions were undertaken by the present authors and the results obtained are embodied in this paper.

MATERIAL AND METHOD

The types of boards included in the study are (i) Flat rectangular (ii) Horizontal curved and (iii) oval with single slit.

The specifications of the different boards are shown in Table I and in Text Figs: 1 - 3.

The horizontal curved boards used are similar to those used by Knake and Whiteleather (*op. cit.*) with slight modifications. The oval board with single slit was made by dimensionally reducing the door described by Matrosov (*op. cit.*) so as to suit the trawler as well as the prevailing fishing conditions. The same net was used with the 3 boards; size of the net being 12.9 m (42.5') described by Satyanarayana *et. al.* (1963).

The trawler used was a small one FISITECH No. VI, Length, 9.75 m; HP, 37. The experiments were conducted in the sea off Cochin during the 1965-66 season, at 5-20 m depths with loose mud bottom.

In the experiments, however, specific depths were chosen namely 10 m, 15m and 20 m and the length of warp correspondingly released were 60 m, 80 m and 110 m. The first series of experiments were conducted at a towing speed of 2 knots which was later raised to 2.5 knots. The method of experimentation was as follows.

At 10 m depth, hauls were made with each type of board keeping the speed and scope-ratio constant for a days operation. The operations of the boards were arranged at random and data for 7 comparable hauls recorded. The experiments were similarly repeated at the other depths. In the second series of experiments, the method adopted was the same but the speed was increased to 2.5 knots.

The horizontal spread between otter boards and the tension in the warps during each haul were recorded. The spread between the doors was measured by the method suggested by Ben yami (1959) and Deshpande (1960). The tension in the warps was estimated by the Tension meter described by Satyanarayana and Nair (1965).

RESULTS

The horizontal spread and the tension in the warps measured are given in Tables II and III.

The average horizontal opening and towing tension noted for each combination of net and otter boards under each depth and speed are given in Table IV.

DISCUSSION

Horizontal opening:

When the curved boards were used, the horizontal spread was found to be relatively high as compared to the other two. The results of the statistical analysis of the data are given in Table V, which will show that the variation between otter boards, towing speeds and scope-ratio are highly significant (0.1% level).

However, the variation between replicates is not significant indicating the availability of more or less constant fishing conditions during the period of experimentation. Among first order interaction, only one (i. e. speed x scope-ratio) interaction is significant (1% level). This interaction may be due to the effect of speed on scope-ratio (Crewe *op. cit.*). None of the second order interaction is significant at 5% level as evidenced from Table V.

In order to examine which among the three otter boards, gives the maximum horizontal opening, Table II has been rearranged by taking the horizontal opening given by the three otter boards under each scope-ratio and towing speed separately. The analysis of variances of these are given in Table VI.

From Table VI, it would be seen that the variation in spread between otter boards are highly significant under each scope-ratio and towing speeds except at scope-

TABLE I GENERAL SPECIFICATIONS OF OTTER BOARDS EXPERIMENTED

| TYPE | Length in cms. | Breadth in cms. | Weight in Kgs. | Area in sq. metres. | Aspect Ratio | Angle of attachment of bridle |
|---------------------------|----------------------|-----------------------|----------------------|---------------------------|-----------------|-------------------------------------|
| Flat rectangular board | 101.60 | 50.80 | 35 | 0.5161 | 0.5 | 37° |
| Horizontal curved board | 101 | 50.50 | 35 | 0.5454 | 0.54 | 30° |
| Oval single slitted board | 100 | 60.00 | 35 | 0.4037 | 0.80 | 42° |

TABLE II HORIZONTAL OPENING OF DIFFERENT PAIRS OF OTTER BOARDS OPERATED UNDER DIFFERENT SCOPE RATIOS AND SPEEDS

| Towing speed in Knots. | Replication Depth/Warp Ratio in Metres > | Horizontal opening in Metres between | | | | | | | | |
|------------------------------|---|--------------------------------------|-------|--------|-------------------------|-------|--------|---------------------------|-------|--------|
| | | Flat Rectangular Board | | | Horizontal curved board | | | Oval single slitted board | | |
| | | 10/60 | 15/80 | 20/110 | 10/60 | 15/80 | 20/110 | 10/60 | 15/80 | 20/110 |
| 2 | 1 | 10.30 | 9.17 | 11.04 | 11.13 | 11.00 | 11.64 | 9.50 | 8.62 | 10.69 |
| | 2 | 9.30 | 10.47 | 11.64 | 11.32 | 11.00 | 11.64 | 9.80 | 9.17 | 10.08 |
| | 3 | 10.02 | 9.60 | 10.44 | 11.53 | 10.65 | 12.25 | 10.05 | 9.12 | 10.08 |
| | 4 | 10.02 | 9.60 | 11.04 | 10.02 | 10.66 | 12.25 | 9.36 | 9.34 | 10.03 |
| | 5 | 10.02 | 10.04 | 10.44 | 11.19 | 10.04 | 12.25 | 9.69 | 7.74 | 10.08 |
| | 6 | 10.47 | 10.04 | 11.04 | 11.64 | 11.56 | 12.25 | 9.69 | 9.17 | 10.03 |
| | 7 | 10.85 | 10.04 | 11.04 | 11.51 | 11.09 | 12.25 | 9.69 | 9.68 | 10.08 |
| 2.5 | 1 | 10.15 | 11.09 | 12.84 | 11.04 | 12.22 | 12.31 | 9.36 | 10.04 | 9.84 |
| | 2 | 10.99 | 10.04 | 10.69 | 11.04 | 11.79 | 13.80 | 9.36 | 10.47 | 12.25 |
| | 3 | 10.99 | 10.21 | 11.98 | 11.43 | 11.53 | 13.20 | 9.82 | 9.60 | 10.65 |
| | 4 | 10.99 | 10.48 | 12.25 | 11.25 | 11.09 | 11.64 | 8.84 | 9.60 | 11.04 |
| | 5 | 10.15 | 10.65 | 11.28 | 11.04 | 11.79 | 12.25 | 8.84 | 10.04 | 10.09 |
| | 6 | 10.02 | 10.65 | 11.64 | 11.25 | 11.79 | 12.84 | 8.73 | 9.60 | 10.44 |
| | 7 | 10.02 | 10.70 | 12.25 | 11.04 | 12.04 | 12.31 | 8.94 | 11.09 | 10.44 |

TABLE III TOWING RESISTANCE OF DIFFERENT OTTER BOARDS OPERATED UNDER DIFFERENT SCOPE RATIOS AND SPEEDS

| Towing speed in knots | Replication | | Towing tension in Kgs. with | | | | | | | |
|-----------------------|-------------------------------|------------------------|-----------------------------|--------|-------------------------|-------|--------|---------------------------|-------|--------|
| | Depth/Warp Length in Metres > | Flat Rectangular Board | | | Horizontal curved board | | | Oval single slitted board | | |
| | | 10/60 | 15/80 | 20/110 | 10/60 | 15/80 | 20/110 | 10/60 | 15/80 | 20/110 |
| 2 | 1 | 295 | 361 | 303 | 242 | 312 | 361 | 264 | 312 | 333 |
| | 2 | 254 | 371 | 322 | 240 | 322 | 342 | 212 | 361 | 333 |
| | 3 | 264 | 342 | 284 | 256 | 401 | 245 | 223 | 236 | 361 |
| | 4 | 294 | 342 | 342 | 326 | 431 | 361 | 264 | 371 | 284 |
| | 5 | 293 | 352 | 284 | 254 | 371 | 245 | 210 | 312 | 361 |
| | 6 | 274 | 284 | 342 | 283 | 264 | 361 | 194 | 381 | 284 |
| | 7 | 210 | 332 | 320 | 284 | 303 | 352 | 254 | 361 | 310 |
| 2.5 | 1 | 264 | 318 | 332 | 294 | 371 | 303 | 336 | 342 | 294 |
| | 2 | 312 | 327 | 303 | 284 | 293 | 331 | 318 | 303 | 371 |
| | 3 | 274 | 312 | 361 | 333 | 322 | 303 | 274 | 361 | 303 |
| | 4 | 293 | 284 | 332 | 312 | 245 | 312 | 401 | 227 | 284 |
| | 5 | 371 | 294 | 264 | 332 | 322 | 312 | 382 | 254 | 245 |
| | 6 | 303 | 303 | 323 | 310 | 312 | 361 | 341 | 236 | 284 |
| | 7 | 332 | 322 | 294 | 294 | 303 | 352 | 323 | 342 | 303 |

TABLE IV AVERAGE HORIZONTAL OPENING AND TOWING TENSION UNDER DIFFERENT OPERATING CONDITIONS

| Depth/warp length in meters | Towing speed in knots | Average horizontal opening in metres | | | Average towing tension in Kgs. (nearest) | | |
|-----------------------------|-----------------------|--------------------------------------|---------------|-------------|--|---------------|-------------|
| | | Flat boards | Curved boards | Oval boards | Flat boards | Curved boards | Oval boards |
| 10/60 | 2.0 | 10.14 | 11.16 | 9.69 | 269 | 256 | 231 |
| | 2.5 | 10.47 | 11.16 | 9.13 | 307 | 308 | 339 |
| 15/80 | 2.0 | 9.85 | 10.86 | 8.93 | 339 | 343 | 333 |
| | 2.5 | 10.54 | 11.75 | 10.06 | 308 | 309 | 295 |
| 20/110 | 2.0 | 10.94 | 12.07 | 10.14 | 313 | 323 | 323 |
| | 2.5 | 11.83 | 12.62 | 10.68 | 315 | 325 | 298 |

TABLE V. ANALYSIS OF VARIANCE OF HORIZONTAL OPENING

| Source of variation | S. S. | D. F. | M. S. |
|------------------------------|----------|-------|------------|
| Total | 143.5045 | 125 | |
| Between otter boards (O. B.) | 70.1717 | 2 | 35.0859 ** |
| Between speeds (S. P.) | 7.4605 | 1 | 7.4605 ** |
| Between scope ratio (S. R.) | 32.1667 | 2 | 16.0834 ** |
| Between replicates (R. P.) | 2.4795 | 6 | 0.4133 |
| O.B × S.P | 0.4401 | 2 | 6.2201 |
| O.B × S.R. | 0.4459 | 4 | 0.1115 |
| O.B × R.P. | 2.9411 | 12 | 0.2451 |
| S.P × S.R. | 5.4533 | 2 | 2.7267 * |
| S.P × R.P. | 1.1584 | 6 | 0.1931 |
| S.R × R.P. | 2.2383 | 12 | 0.1866 |
| O.B × S.P. × S.R. | 1.5107 | 4 | 0.3777 |
| O B × S.P. × R.P. | 2.1679 | 12 | 0.1807 |
| O.B × S.R. × R.P. | 3.3591 | 24 | 0.1493 |
| S.P × S.R. × R.P. | 3.7232 | 12 | 0.3101 |
| O.B × S.R. × S.P. × R. P. | 7.881 | 24 | 0.3245 |

* Denotes significance at 1% level.

** Denotes significance at 0.1% level

ratio of 20/110 and speed 2.5 knots. On comparing their means it can be observed that the curved board gives significantly (5% Level) higher lateral opening in comparison with the other two.

Towing resistance:

Since the gear and fishing conditions are similar, the difference in tension may be attributed to the difference in the otter boards used. From Table IV, it would be seen that though the resistance of otter boards operated with gear do not show appreciable difference, the oval otter boards in general gave lesser resistance, while the curved board recorded more and the flat one coming in between. The analysis of variance on the resistance data is given in Table VII.

It can be seen from the table that the variation in tension between otter boards, between speeds and between replications are not significant at 5% level. But the

variation between scope ratios is high significant (0.1% level). Also as in the case of horizontal opening the first order interaction scope-ratio x speed, shows a very high significant variation (0.1% level). This may be due to the effect of speed on scope-ratio. It is difficult to interpret the highly significant second order interaction between OB X SR X SP and a possible reason for its significance may be due to the high interacting effect of speed and scope ratio.

Summarising this communication incorporates the results of comparative fishing experiments conducted off Cochin with (i) Rectangular (ii) Horizontal curved and (iii) oval otter boards. The experiments were conducted at three different depths and at two different speeds. The towing resistance on the warps and horizontal opening of the boards were taken as indices in evaluating the efficiency and the following results were

TABLE VI ANALYSIS OF VARIANCE OF HORIZONTAL OPENING UNDER
DIFFERENT SCOPE RATIOS AND SPEEDS

| Towing speed | | 200 Knots | | | | | | 2.5 Knots | | | | | |
|-------------------------|--------------------|-----------|--------|---------|--------|---------|--------|-----------|--------|---------|--------|---------|--------|
| Scope ratio | | 10/60 | | 15/80 | | 20/110 | | 10/60 | | 15/80 | | 20/110 | |
| Source of variation | Degrees of freedom | S. S. | M. S. | S. S. | M. S. | S. S. | M. S. | S. S. | M. S. | S. S. | M. S. | S. S. | M. S. |
| Total | 2 | 11.8610 | — | 17.0593 | — | 14.9604 | — | 19.1892 | — | 13.9427 | — | 23.1716 | — |
| Between otter boards | 2 | 8.3774 | 4.1887 | 12.3356 | 6.1678 | 13.0603 | 6.5302 | 16.0641 | 8.0321 | 10.5698 | 5.2849 | 13.3100 | 6.6550 |
| Residual | 18 | 3.4836 | 0.1935 | 4.7237 | 0.2642 | 1.9001 | 0.1056 | 3.1251 | 0.1736 | 3.3729 | 0.1872 | 9.8626 | 0.5479 |
| Critical difference | | 0.4941 | | 0.5754 | | 0.3651 | | 0.4679 | | 0.4877 | | 0.8310 | |
| Mean Horizontal opening | | | | | | | | | | | | | |
| Flat board | | 10.1400 | | 9.8514 | | 10.9543 | | 10.4729 | | 10.5457 | | 11.8471 | |
| Curved board | | 11.1914 | | 10.8571 | | 12.0757 | | 11.1557 | | 11.7500 | | 12.6214 | |
| Oval board | | 9.6829 | | 8.9814 | | 10.1529 | | 9.0557 | | 10.0629 | | 10.6843 | |

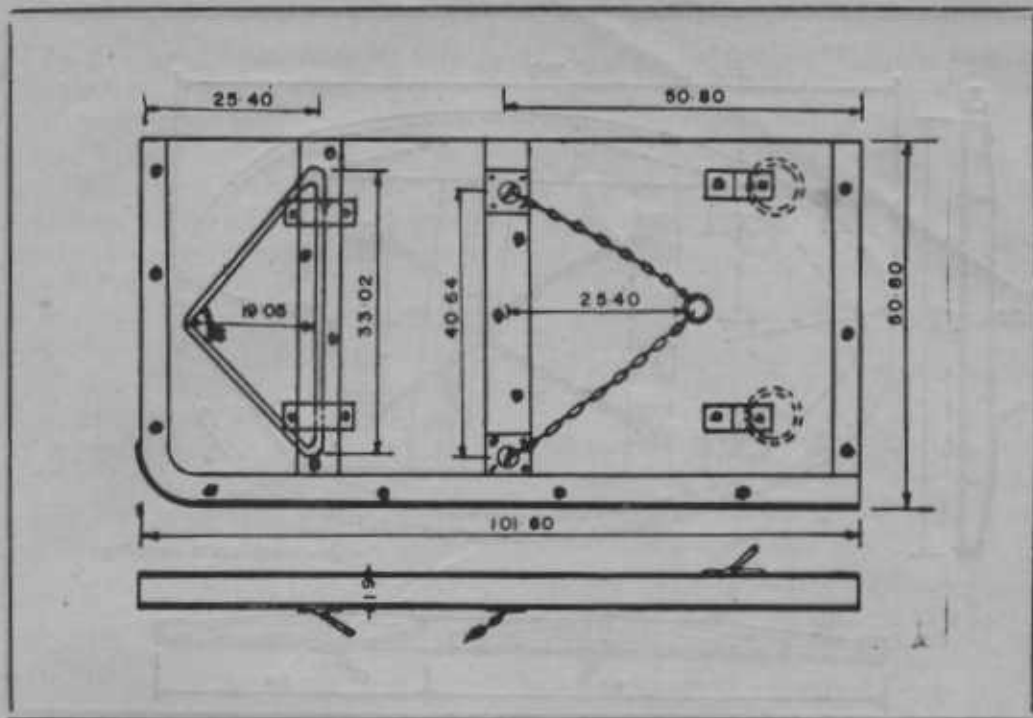


Fig I Design details of common flat rectangular otter board

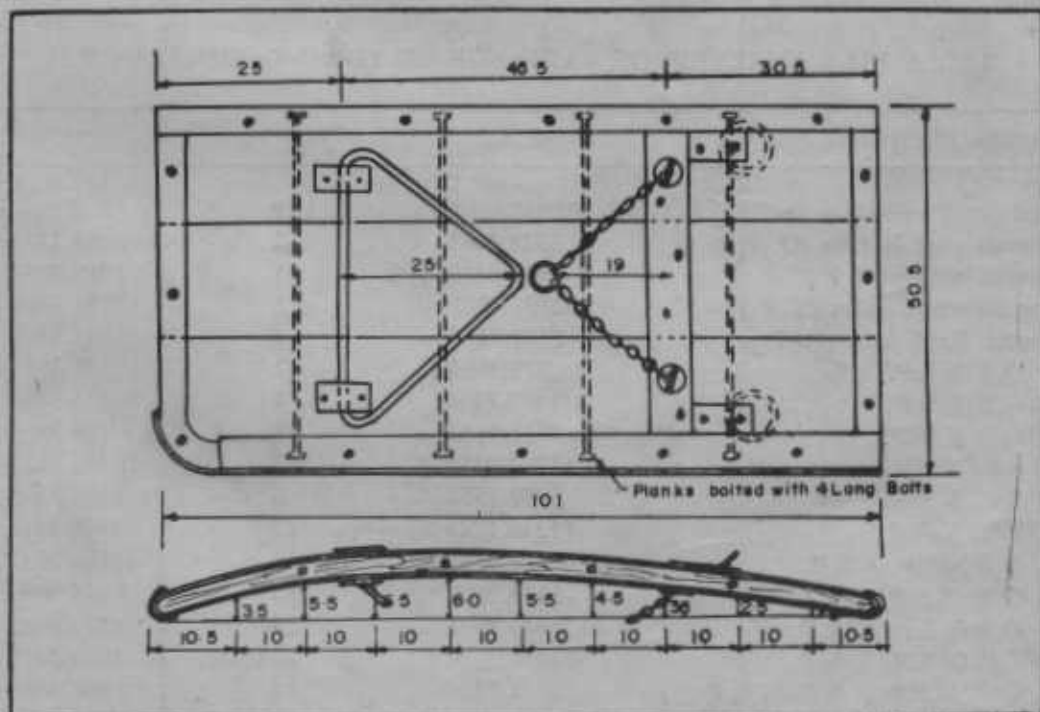


Fig II Design details of Horizontal curved otter board

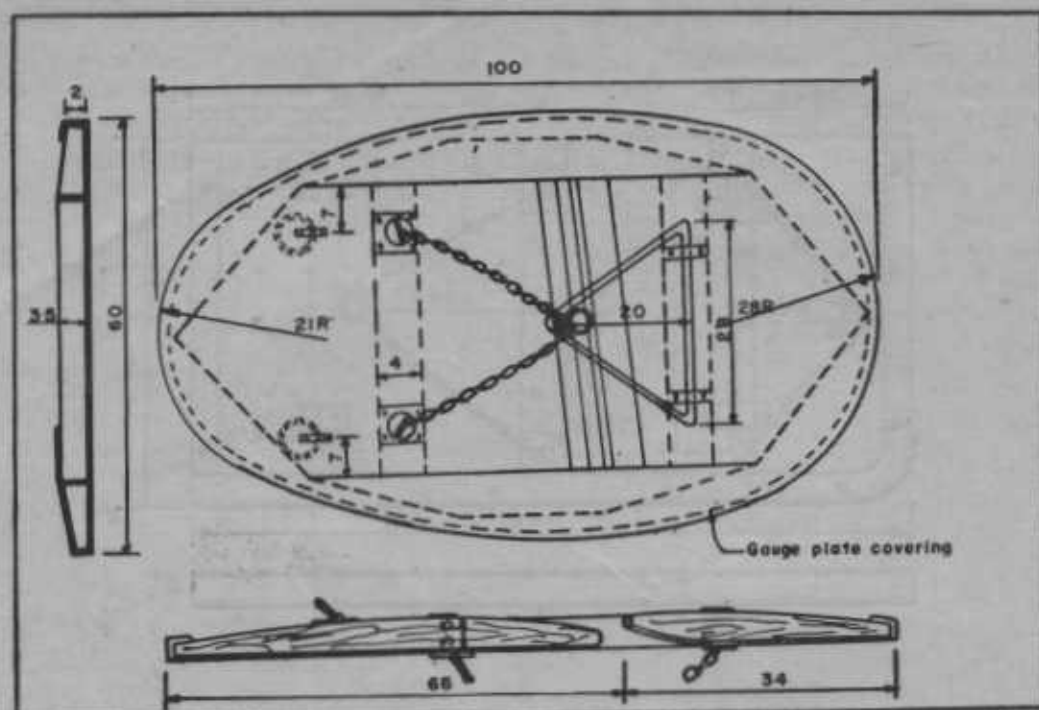


Fig 3 Design details of oval, single slitted otter board

TABLE VII. ANALYSIS OF VARIANCE OF TOWING RESISTANCE.

| Source of variation | S. S. | D. F. | M. S. |
|------------------------------|-------------|-------|--------------|
| Total | 255033.6588 | 125 | |
| Between otter boards (O. B.) | 1328.4445 | 2 | 664.2223 |
| Between speeds (S. P.) | 1913.3413 | 1 | 1913.3413 |
| Between scope ratios (S. R.) | 32707.4921 | 2 | 16353.7461 * |
| Between Replicates (R. P.) | 2501.8255 | 6 | 416.9709 |
| O. B X S.P. | 773.3968 | 2 | 386.6984 |
| O. B X S.R. | 1503.7936 | 4 | 375.9484 |
| O. B X R.P. | 4827.5555 | 12 | 402.2963 |
| S.P. X S.R. | 56912.8254 | 2 | 28456.4127 * |
| S.P. X R.P. | 6989.1587 | 6 | 1164.8598 |
| S.R. X R.P. | 15319.1745 | 12 | 1609.9312 |
| O. B X S.P. X S.R. | 40805.1746 | 4 | 10201.2937 ° |
| O. B. X S.P. X R.P. | 5603.2698 | 12 | 466.9392 |
| O. B X S.R. X R.P. | 36649.8731 | 24 | 1522.9113 |
| S.P. X S.R. X R.P. | 22456.5080 | 12 | 1871.3757 |
| O. B. X S.P. X S.R. X R.P. | 20841.8254 | 24 | 868.4083 |

° Denotes significance at 0.1% level.

observed. The horizontal opening (significant at 5% level) of the net operated with curved otter board was high when compared with the other two. In general the oval board gave lesser resistance while the curved board offered more and the flat coming in between. The variation in tension between the boards, speeds and replicates were not significant at 5% level.

ACKNOWLEDGEMENT

The authors express their sincere thanks to Dr. A. N. Bose, Director, and Shri G. K. Kuriyan, Senior Research Officer, (Graft & Gear), Central Institute of Fisheries Technology, Ernakulam-Cochin for their keen interest and valuable suggestions during the course of this investigation.

REFERENCES

- Ben-yami. 1959. Modern fishing gear of the world. Fishing News (Books) Ltd., London, pp. 213-227.
- Ben-yami. 1963. Technical report No. 11, 65
- Crewe, P. R. 1963. Modern fishing gear of the world. Fishing news (Books) Ltd., London. pp. 165-181.
- Dale, P and Moller, S. 1963. *Ibid* pp. 482-489.
- Deshpande, S. D. 1960. *Indian J. Fish* VII 2, 458.
- Dickson, W, 1959. Modern fishing gear of the world. Fishing news (Books) Ltd., London. pp. 166-174.

- Knake, B. O. and Whiteleather, R. T. 1944. *Fishery leaflet* No. 49 U. S. Department of Interior Fish & Wild life service, Washington D. C.
- Luigi Catasta. 1959. Modern Fishing gear of the world. Fishing News (Books) Ltd., London pp. 251-253
- Matrasov, I. R. 1958. *Rybnoe Khozyaystvo* 34, 9, 40.
- Satyanarayana, A. V. V., Kuriyan, G. K. & Nair, R. S. 1963 *Proc. Indo-Pac. Fish. Coun.* 10, 2, 226.
- Satyanarayana, A. V. V. and Mukundan, M. 1963. Studies on otter boards—Angle of attachment of the bridles. (under publication)
- Scharfe, J. 1959. Modern fishing gear of the world. Fishing news (Books) Ltd., London, pp. 245-247.
- Scharfe, J. 1959. *Studies and Review* No. 6 General council for the Mediterranean.
- Sevastianov, V. V. 1955. *Tudy VNIRO*, 30, p. 57.
- Suberkrub, F. 1959. Modern fishing gear of the world. Fishing news (Books) Ltd., London. pp. 259-360
- Takayama, S. and Koyama, T. 1958. *Bull. Tokai. Reg. Fish. Res. Lab.* No. 22, 37.
- Takayama, S. and Koyama, T. 1961. *Ibid*, No. 31, 297.
- Yakovliev, A. I. 1955. *Tudy, VNIRO*, 30, 61.